

# Numerical modelling of large amplitude long waves in the coastal zone using COULWAVE code

Tomas Torsvik

Bergen Center for Computational Science  
UNIFOB  
University of Bergen

Guadeloupe  
February 2008

# Bergen, Norway



# Overview

- Basic equations
  - Nonlinear equations
  - Dispersive equations
- Properties of the COULWAVE model
  - Boundary conditions:
    - Open boundaries
    - Wetting/drying along the coast line
  - Wave breaking
  - Bottom friction
- Examples
  - Breaking and non-breaking wave runup
  - Simulation using realistic wave fields and bathymetry
  - Ship waves

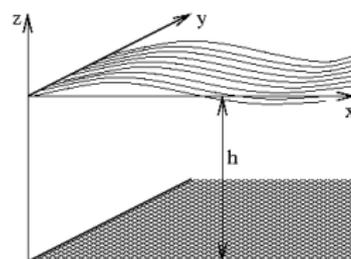
## Equations for inviscid, incompressible flow

- Continuity equation:

$$\nabla \cdot \mathbf{u} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

- Euler equation:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \mathbf{g}$$



- Dynamic and kinematic boundary conditions:

$$p = p_a(x, y, t), \quad \text{at } z = \eta(x, y, t)$$

$$w = \frac{\partial \eta}{\partial t} + u \frac{\partial \eta}{\partial x} + v \frac{\partial \eta}{\partial y}, \quad \text{at } z = \eta(x, y, t)$$

$$w = u \frac{\partial h}{\partial x} + v \frac{\partial h}{\partial y}, \quad \text{at } z = -h(x, y)$$

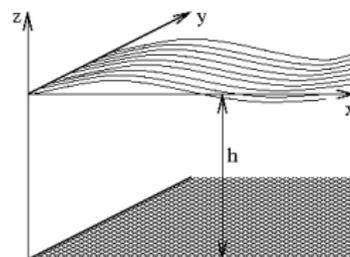
## Equations for inviscid, incompressible flow

- Continuity equation:

$$\nabla \cdot \mathbf{u} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

- Euler equation:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \mathbf{g}$$



- Dynamic and kinematic boundary conditions:

$$p = p_a(x, y, t), \quad \text{at } z = \eta(x, y, t)$$

$$w = \frac{\partial \eta}{\partial t} + u \frac{\partial \eta}{\partial x} + v \frac{\partial \eta}{\partial y}, \quad \text{at } z = \eta(x, y, t)$$

$$w = u \frac{\partial h}{\partial x} + v \frac{\partial h}{\partial y}, \quad \text{at } z = -h(x, y)$$

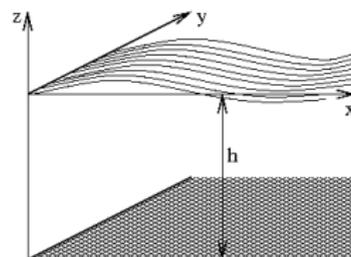
## Equations for inviscid, incompressible flow

- Continuity equation:

$$\nabla \cdot \mathbf{u} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

- Euler equation:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \mathbf{g}$$



- Dynamic and kinematic boundary conditions:

$$p = p_a(x, y, t), \quad \text{at } z = \eta(x, y, t)$$

$$w = \frac{\partial \eta}{\partial t} + u \frac{\partial \eta}{\partial x} + v \frac{\partial \eta}{\partial y}, \quad \text{at } z = \eta(x, y, t)$$

$$w = u \frac{\partial h}{\partial x} + v \frac{\partial h}{\partial y}, \quad \text{at } z = -h(x, y)$$

# Linear wave theory

- Use linearized equations and assume a wave solution:

$$\eta = \eta_{max} \sin(kx - \omega t)$$

- Dispersion relation for linear wave:

$$\omega^2 = gk \tanh(kh)$$

- Phase velocity:

$$c = \frac{\omega}{k} = \left( \frac{g}{k} \tanh(kh) \right)^{1/2}$$

# Linear wave theory

- Use linearized equations and assume a wave solution:

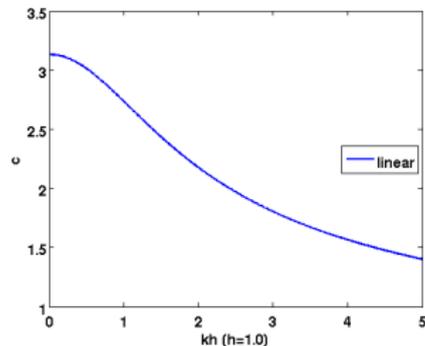
$$\eta = \eta_{max} \sin(kx - \omega t)$$

- Dispersion relation for linear wave:

$$\omega^2 = gk \tanh(kh)$$

- Phase velocity:

$$c = \frac{\omega}{k} = \left( \frac{g}{k} \tanh(kh) \right)^{1/2}$$



# Shallow water approximation

- For  $kh \rightarrow 0$ 
  - Dispersion relation:

$$\omega^2 \approx gk^2 h$$

- Phase speed:

$$c = \sqrt{gh}$$

- Long waves are non-dispersive.
  - The wave energy is transported with the individual waves, i.e. there is little or no exchange of wave energy between waves in a wave train propagating in shallow water.

# Shallow water approximation

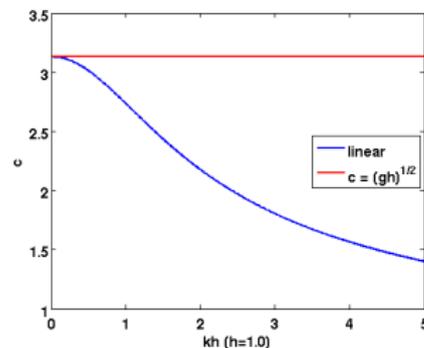
- For  $kh \rightarrow 0$ 
  - Dispersion relation:

$$\omega^2 \approx gk^2 h$$

- Phase speed:

$$c = \sqrt{gh}$$

- Long waves are non-dispersive.
- The wave energy is transported with the individual waves, i.e. there is little or no exchange of wave energy between waves in a wave train propagating in shallow water.



# Shallow water approximation

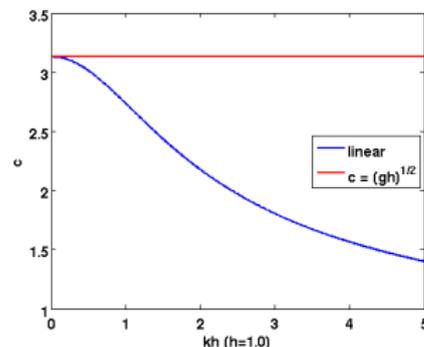
- For  $kh \rightarrow 0$ 
  - Dispersion relation:

$$\omega^2 \approx gk^2 h$$

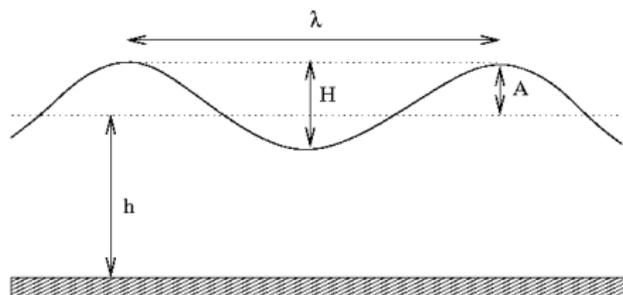
- Phase speed:

$$c = \sqrt{gh}$$

- Long waves are non-dispersive.
- The wave energy is transported with the individual waves, i.e. there is little or no exchange of wave energy between waves in a wave train propagating in shallow water.



## Scales for surface gravity waves



Acceleration scale:

$g$  - acceleration of gravity

Length scales:

$\lambda$  - wave length,  $h$  - depth,  $A$  - amplitude/elevation

Time scale:

Usually constructed from length and acceleration scales, e.g.

$$t = \lambda / \sqrt{gh}$$

## Approximations for shallow water flow

Shallow water, long wave theory:  $\epsilon = \frac{h}{\lambda} \ll 1$

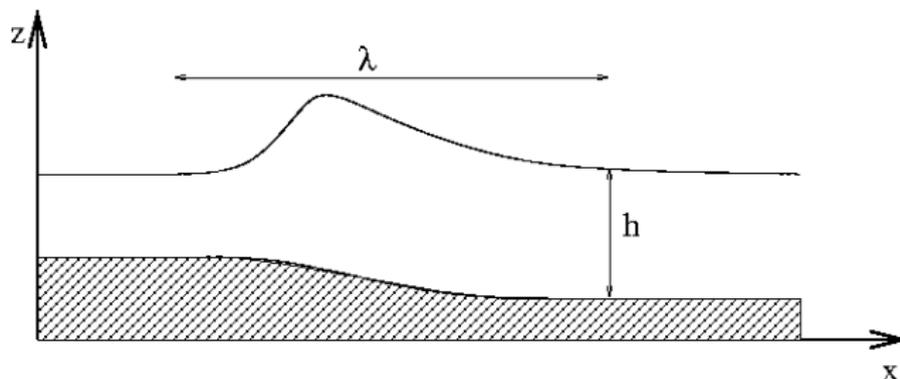
Weakly non-linear theory:  $\mu = \frac{A}{h}, \frac{A}{\lambda} \ll 1$

Ursell number:  $Ur = \frac{\epsilon}{\mu^2} = \frac{A\lambda^2}{h^3}$

- Linear theory:  $Ur \ll 1$
- Weakly dispersive, weakly non-linear waves:  $Ur \approx 1$
- Non-dispersive, finite amplitude waves:  $Ur \gg 1$

Comparison of length scales indicates if waves are non-linear or dispersive, or if both effects should be included.

# Shallow water theory



2D case discussed for simplicity

$U$ ,  $W$  - characteristic horizontal and vertical velocities

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0 \Rightarrow \frac{W}{h} \sim \frac{U}{\lambda} \Rightarrow \frac{W}{U} \sim \frac{h}{\lambda} \ll 1$$

## Strategies for numerical simulations

Numerical solution of Euler equations is possible, but at high computational cost.

- Restrict computational domain (or resolution)

Shallow water approximation:

- Reduce 3D equations to 2D equations by integrating over depth.
  - Derive governing equations by expanding  $\mathbf{u}$  in terms of  $z$ .
- Several different formulations may be derived from the primitive equations.

## Korteweg-de Vries equation

Simplest form of weakly nonlinear, weakly dispersive equation:

$$\frac{\partial \eta}{\partial t} + \left(1 + \frac{3}{2}\eta\right) \frac{\partial \eta}{\partial x} + \frac{1}{6} \frac{\partial^3 \eta}{\partial x^3} = 0$$

Compare with properties for the nonlinear transport equation

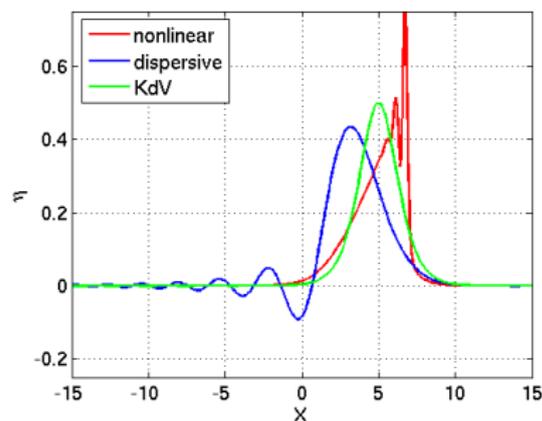
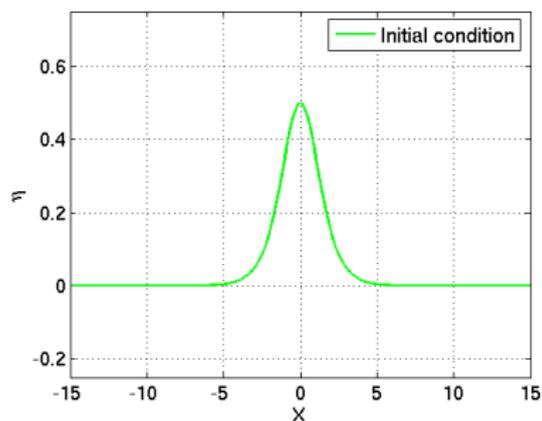
$$\frac{\partial \eta}{\partial t} + \left(1 + \frac{3}{2}\eta\right) \frac{\partial \eta}{\partial x} = 0$$

and the linear weakly dispersive equation

$$\frac{\partial \eta}{\partial t} + \frac{\partial \eta}{\partial x} + \frac{1}{6} \frac{\partial^3 \eta}{\partial x^3} = 0$$

# Korteweg-de Vries equation (Cont.)

Evolution of an initial disturbance  $\eta = A \cosh^{-2} \left[ \frac{\sqrt{3A}}{2} x \right]$



## fKdV and KP equations

Forced KdV (fKdV) equation (1D propagation)

$$\frac{\partial \eta}{\partial t} + \left(1 + \frac{3}{2}\eta\right) \frac{\partial \eta}{\partial t} + \frac{1}{6} \frac{\partial^3 \eta}{\partial x^3} = \frac{1}{2} \frac{\partial p}{\partial x}$$

Kadomtsev-Petviashvili (KP) equation (2D propagation)

$$\frac{\partial}{\partial x} \left[ \frac{\partial \eta}{\partial t} + \left(1 + \frac{3}{2}\eta\right) \frac{\partial \eta}{\partial t} + \frac{1}{6} \frac{\partial^3 \eta}{\partial x^3} \right] - \frac{1}{2} \frac{\partial^2 \eta}{\partial y^2} = \frac{1}{2} \frac{\partial^2 p}{\partial x^2}$$

Derived from KdV equation by relaxing 1D requirement.

## Boussinesq equations

- Formulate equations in terms of depth averaged velocity  $\bar{\mathbf{u}}$ , where  $\nabla_H = (\partial/\partial x, \partial/\partial y)$ .
- Continuity equation:

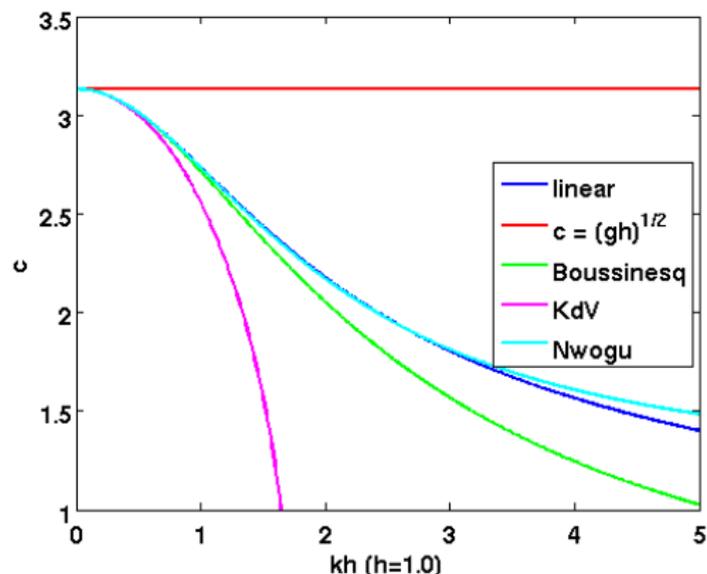
$$\frac{\partial \eta}{\partial t} + \nabla_H \cdot [(h + \eta)\bar{\mathbf{u}}] = 0$$

- Momentum equation:

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + (\bar{\mathbf{u}} \cdot \nabla_H)\bar{\mathbf{u}} = -\nabla_H \eta - \nabla_H p_a + \frac{1}{3}h^2 \nabla_H \nabla_H \cdot \left( \frac{\partial \bar{\mathbf{u}}}{\partial t} \right)$$

- Formulations with depth variation include  $\nabla_H h$  terms.
- Higher order formulations include dispersive terms with nonlinear corrections.

# Dispersion relation for long wave equations



Linear:  $c = \sqrt{(g/k) \tanh(kh)}$

Boussinesq: Classical Boussinesq formulation

Nwogu: Improved Boussinesq formulation

# Properties of long wave equations

KdV and KP equations:

- + Closed form (explicit) solutions exist for solitary and periodic waves.
- Restricted to unidirectional (KdV) or narrow angle (KP) of wave propagation.
- Poor dispersion relation for intermediate water depth.

Boussinesq equations:

- No known closed form solutions.
- + No preferred direction of wave propagation.
- + Improved formulation with reasonable dispersion relation up to  $kh \approx \pi$ .

## The COULWAVE model

- **COULWAVE: Cornell University Long Wave model**  
`http://ceprofs.tamu.edu/plynett/COULWAVE/`
- Boussinesq type model equations
- High order predictor-corrector method (Adams-Bashforth + Adams-Moulton) for time stepping
- Spatial derivatives approximated by finite differences
- Equations discretized on a uniform, quadrilateral grid
- Depth a function of space and time  $h = h(\mathbf{x}, t)$ , which allows simulation of underwater landslide
- **FUNWAVE: Long wave model similar to COULWAVE**  
`http://chinacat.coastal.udel.edu/~kirby/programs/funwave/funwave.html`

## Continuity equation

$$\begin{aligned}
 & \frac{1}{\epsilon} \frac{\partial h}{\partial t} + \frac{\partial \eta}{\partial t} + \nabla \cdot [(h + \epsilon \eta) \bar{\mathbf{u}}] \\
 & - \mu^2 \nabla \cdot \left\{ \left[ \frac{h^3 + \epsilon^3 \eta^3}{6} - \frac{(h + \epsilon \eta) z_\alpha^2}{2} \right] \nabla S \right. \\
 & \left. - \left[ \frac{h^2 - \epsilon^2 \eta^2}{2} + (h + \epsilon \eta) z_\alpha \right] \nabla T \right\} = \mathcal{O}(\mu^4)
 \end{aligned} \tag{1}$$

where

$$\mathbf{S} = \nabla \cdot \bar{\mathbf{u}}, \quad T = \nabla \cdot (h \bar{\mathbf{u}}) + \frac{1}{\epsilon} \frac{\partial h}{\partial t}$$

and  $z_\alpha$  is a reference depth, usually  $z_\alpha = -0.531h$

## Momentum equation

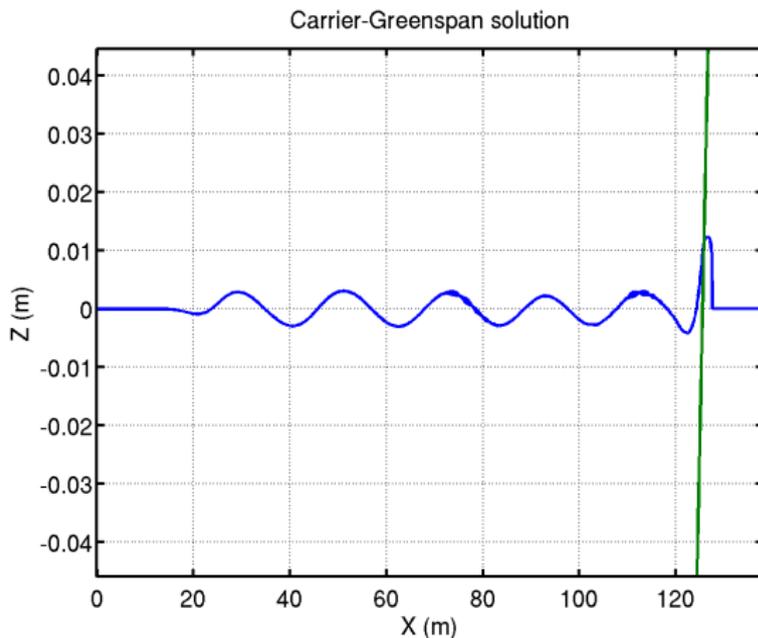
$$\begin{aligned}
 & \frac{\partial \bar{\mathbf{u}}}{\partial t} + \epsilon \bar{\mathbf{u}} \cdot \nabla \bar{\mathbf{u}} + \nabla \eta + \nabla p_a + \mu^2 \frac{\partial}{\partial t} \left\{ \frac{z_\alpha^2}{2} \nabla S + z_\alpha \nabla T \right\} \\
 & + \epsilon \mu^2 \left[ (\bar{\mathbf{u}} \cdot \nabla z_\alpha)(z_\alpha \nabla S + \nabla T) + z_\alpha \nabla (\bar{\mathbf{u}} \cdot \nabla T) + \frac{z_\alpha^2}{2} \nabla (\bar{\mathbf{u}} \cdot \nabla S) \right] \\
 & + \epsilon \mu^2 \left[ T \nabla T - \nabla \left( \eta \frac{\partial T}{\partial t} \right) \right] \\
 & + \epsilon^2 \mu^2 \nabla \left( \eta S T - \frac{\eta^2}{2} \frac{\partial S}{\partial t} - \eta \bar{\mathbf{u}} \cdot \nabla T \right) \\
 & + \epsilon^3 \mu^2 \nabla \left[ \frac{\eta^2}{2} (S^2 - \bar{\mathbf{u}} \cdot \nabla S) \right] = \mathcal{O}(\mu^4)
 \end{aligned}
 \tag{2}$$

# Boundary conditions

- Open boundaries: Flow Relaxation Zones (Sponge Layer)
  - Multiply  $\bar{\mathbf{u}}$  by exponentially decaying function near open boundaries.
- Closed boundaries: Full reflection of waves approaching the boundary
- Wet-dry boundary: Moving boundary at the shore line
  - Linear extrapolation of water phase into dry region

## Example: Carrier-Greenspan solution

- Carrier-Greenspan solution for runup and rundown on a plane beach
- Wave height 0.006 m, period 10 s, depth 0.5 m, slope 1:25



## Wave breaking

- Wave breaking model after Kennedy et al. (2000)<sup>1</sup>
- Add an eddy viscosity term to the momentum equation.

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + \epsilon \bar{\mathbf{u}} \cdot \nabla_H \bar{\mathbf{u}} + \nabla_H \eta + \nabla_H p_a - \frac{1}{3} \mu^2 h^2 \nabla_H \nabla_H \cdot \left( \frac{\partial \bar{\mathbf{u}}}{\partial t} \right) - \mathbf{R}_b(\nu) = \mathcal{O}(\mu^4)$$

- Eddy viscosity:  $\nu = B \delta_b^2 (h + \eta) \eta_t$   
 $\delta_b$  - nondimensional mixing length, usually  $0.9 < \delta_b < 1.5$

<sup>1</sup>J. Waterway, Port, Coastal, and Ocean Eng. (39), 2000 

## Wave breaking (cont.)

- Breaking occurs when  $\eta_t > \eta_t^*$

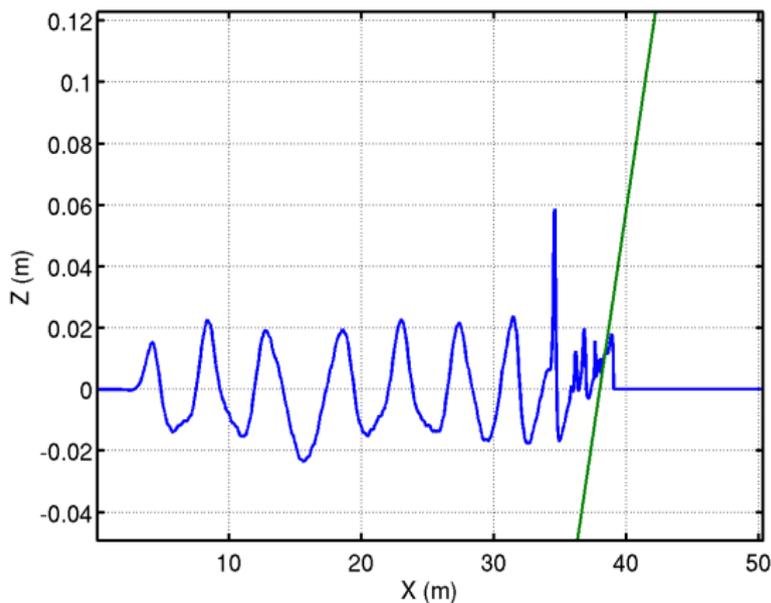
$$B = \begin{cases} 1, & \eta_t \geq 2\eta_t^* \\ \eta_t/\eta_t^* - 1, & \eta_t^* \leq \eta_t < 2\eta_t^* \\ 0, & \eta_t < \eta_t^* \end{cases}$$

- Once triggered,  $\eta_t^*$  decreases with time from  $\eta_t^{*(l)}$  to  $\eta_t^{*(F)}$

$$\eta_t^* = \begin{cases} \eta_t^{*(l)} + \frac{t - t_0}{T^*} (\eta_t^{*(F)} - \eta_t^{*(l)}), & 0 \leq (t - t_0) < T^* \\ \eta_t^{*(F)}, & (t - t_0) \geq T^* \end{cases}$$

## Example: Waves breaking on a plane beach

- Regular waves breaking on a beach
- Wave height 0.036 m, depth 0.36 m, slope 1:34.26



# Bottom friction

- Bottom friction formulations:
  - Standard quadratic formulation

$$R = C_{FR} \bar{\mathbf{u}} |\bar{\mathbf{u}}|$$

- Convolution integral formulation

$$R = C_{FR} \int_0^t \frac{\nabla_H \cdot \bar{\mathbf{u}}}{\sqrt{t - \tau}} d\tau$$

## Bottom friction: Standard formulation

- Boussinesq equations with standard bottom friction formulation  
Continuity equation:

$$\frac{\partial \eta}{\partial t} + \nabla_H \cdot [(h + \epsilon \eta) \bar{\mathbf{u}}] = \mathcal{O}(\mu^4)$$

Momentum equation:

$$\begin{aligned} & \frac{\partial \bar{\mathbf{u}}}{\partial t} + \epsilon \bar{\mathbf{u}} \cdot \nabla_H \bar{\mathbf{u}} + \nabla_H \eta + \nabla_H p_a \\ & - \frac{1}{3} \mu^2 h^2 \nabla_H \nabla_H \cdot \left( \frac{\partial \bar{\mathbf{u}}}{\partial t} \right) + C_{FR} \bar{\mathbf{u}} |\bar{\mathbf{u}}| = \mathcal{O}(\mu^4) \end{aligned}$$

## Bottom friction: Convolution integral formulation

- Viscous effects can be important near solid boundaries.
- Boussinesq equations with a bottom friction derived from boundary layer analysis (Liu and Orfila<sup>2</sup>):

$$\frac{\partial \eta}{\partial t} + \nabla_H \cdot [(h + \epsilon \eta) \bar{\mathbf{u}}] - \frac{\delta}{\mu \sqrt{\pi}} \int_0^t \frac{\nabla_H \cdot \bar{\mathbf{u}}}{\sqrt{t - \tau}} d\tau = \mathcal{O}(\mu^4)$$

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + \epsilon \bar{\mathbf{u}} \cdot \nabla_H \bar{\mathbf{u}} + \nabla_H \eta + \nabla_H p_a - \frac{1}{3} \mu^2 h^2 \nabla_H \nabla_H \cdot \left( \frac{\partial \bar{\mathbf{u}}}{\partial t} \right) = \mathcal{O}(\mu^4)$$

$$\delta^2 = \frac{\nu}{\lambda \sqrt{gh}}, \quad \mathcal{O}(\delta) \approx \mathcal{O}(\mu^4) \approx \mathcal{O}(\epsilon^2)$$

<sup>2</sup>J. Fluid Mech.(2004), vol. 520

# Approximation of convolution integral

- Large computational cost for computing the exact convolution integral.
- We can estimate the value of the convolution integral by

$$\int_{t-t^*}^t \frac{\nabla_H \cdot \bar{\mathbf{u}}}{\sqrt{t-\tau}} d\tau + C_R R(t-t^*)$$

where  $t^*$  is the truncation time,  $R(t-t^*)$  is a time dependent residual term, and  $C_R$  is the residual coefficient.

# Approximation of convolution integral

- Large computational cost for computing the exact convolution integral.
- We can estimate the value of the convolution integral by

$$\int_{t-t^*}^t \frac{\nabla_H \cdot \bar{\mathbf{u}}}{\sqrt{t-\tau}} d\tau + C_R R(t-t^*)$$

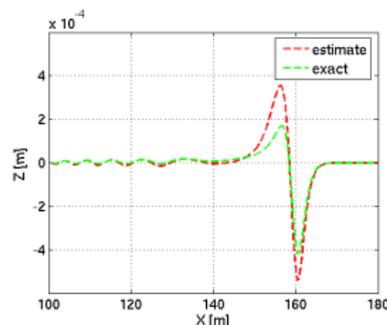
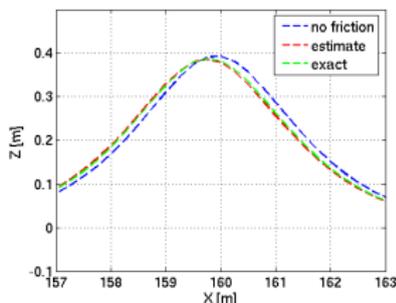
where  $t^*$  is the truncation time,  $R(t-t^*)$  is a time dependent residual term, and  $C_R$  is the residual coefficient.

## Approximation of convolution integral

- Large computational cost for computing the exact convolution integral.
- We can estimate the value of the convolution integral by

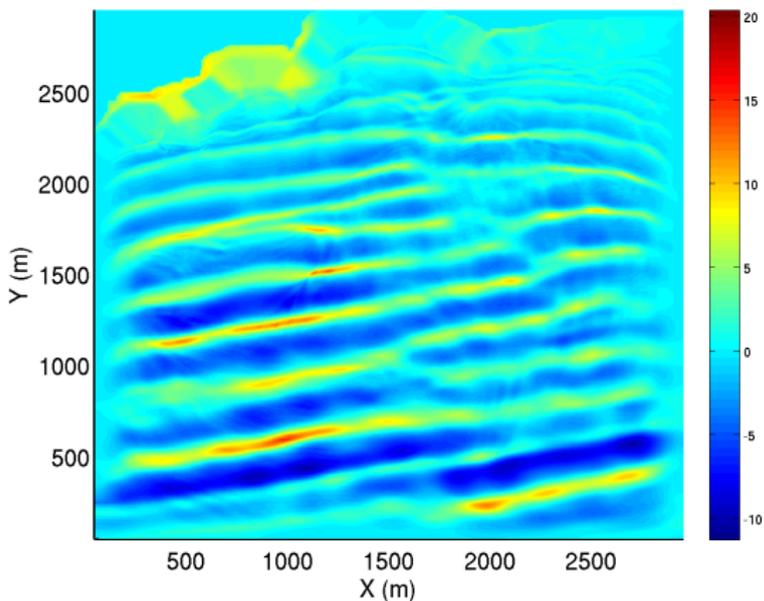
$$\int_{t-t^*}^t \frac{\nabla_H \cdot \bar{\mathbf{u}}}{\sqrt{t-\tau}} d\tau + C_R R(t-t^*)$$

where  $t^*$  is the truncation time,  $R(t-t^*)$  is a time dependent residual term, and  $C_R$  is the residual coefficient.



## Example: Complex topographies

- Simulating irregular wave train in Wiamea Bay, Hawaii



## Example: Wash waves from high speed vessels



### HSS "Stena Discovery"

Top Speed:

40 knots (= 20.6 m/s)

Dimensions:

Length: 121.75 m

Width: 40.00 m

Draft: 4.80 m

- Waves from high speed vessels:
  - Long wave lengths and wave periods.
  - Large wave energy.
  - Qualitatively different from waves generated by conventional ships.
- Potentially dangerous for people on the shore or in small boats.
- May damage structures at the shore or moored vessels.
- May increase erosion and disturb marine habitats.

## Example: Wash waves from high speed vessels



HSS “Stena Discovery”

Top Speed:

40 knots (= 20.6 m/s)

Dimensions:

Length: 121.75 m

Width: 40.00 m

Draft: 4.80 m

- Waves from high speed vessels:
  - Long wave lengths and wave periods.
  - Large wave energy.
  - Qualitatively different from waves generated by conventional ships.
- Potentially dangerous for people on the shore or in small boats.
- May damage structures at the shore or moored vessels.
- May increase erosion and disturb marine habitats.

## Example: Wash waves from high speed vessels



### HSS "Stena Discovery"

Top Speed:

40 knots (= 20.6 m/s)

Dimensions:

Length: 121.75 m

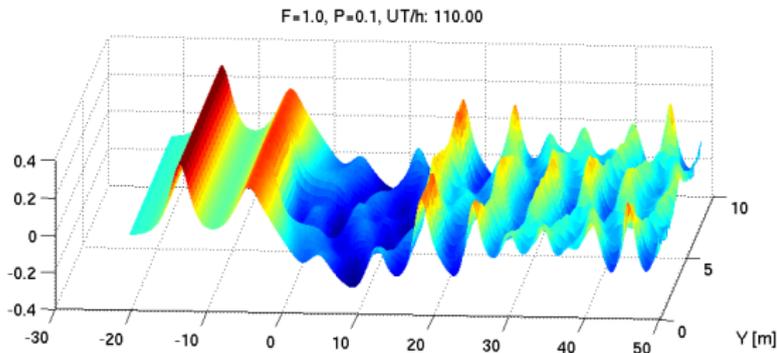
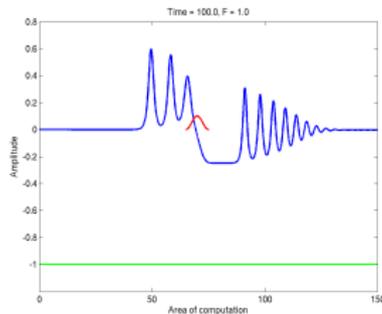
Width: 40.00 m

Draft: 4.80 m

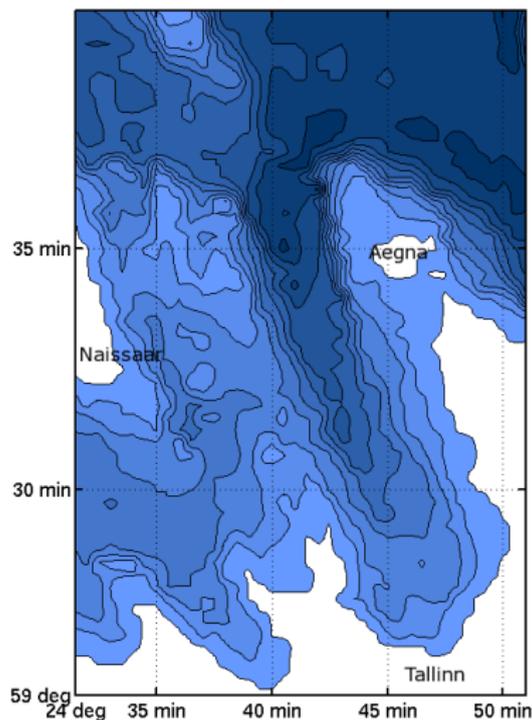
- Waves from high speed vessels:
  - Long wave lengths and wave periods.
  - Large wave energy.
  - Qualitatively different from waves generated by conventional ships.
- Potentially dangerous for people on the shore or in small boats.
- May damage structures at the shore or moored vessels.
- May increase erosion and disturb marine habitats.

## Waves generated by a pressure disturbance

- Pressure included through dynamic boundary condition. Consistent with primitive equations.
- Simple to implement.
- Difficult to represent specific hull shapes.

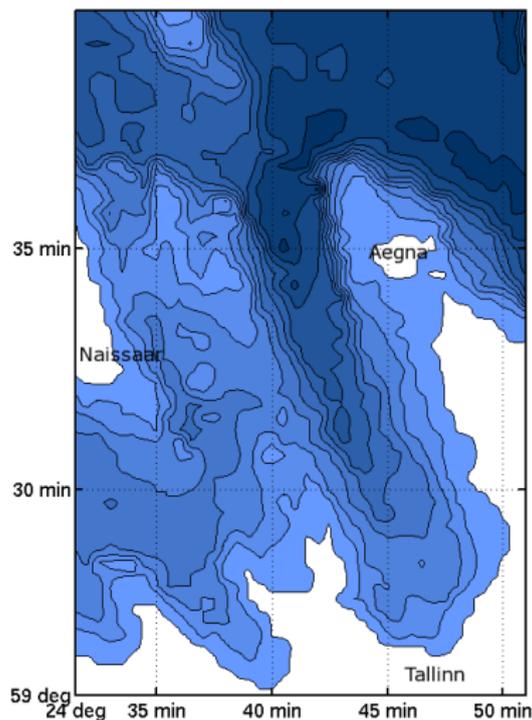


## Ship waves in Tallinn Bay



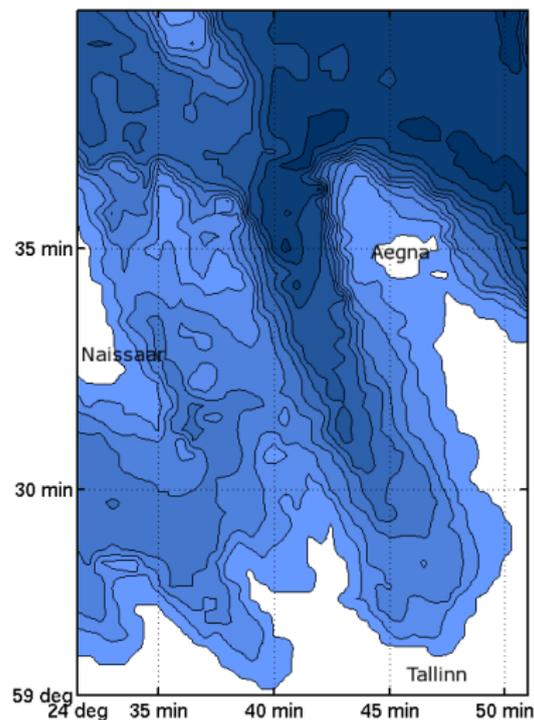
- Basin of about 10 km x 20 km
- Ship traffic follows NW - SE underwater valley, with depth ranging from 10 m to 90 m.
- Daily crossings (ingoing or outgoing)
  - 22 HSC/Catamaran
  - 8-10 Hydrofoil
- A natural laboratory for the study of long waves.
  - Also relevant for tsunami research.

## Ship waves in Tallinn Bay



- Basin of about 10 km x 20 km
- Ship traffic follows NW - SE underwater valley, with depth ranging from 10 m to 90 m.
- Daily crossings (ingoing or outgoing)
  - 22 HSC/Catamaran
  - 8-10 Hydrofoil
- A natural laboratory for the study of long waves.
  - Also relevant for tsunami research.

## Ship waves in Tallinn Bay



- Basin of about 10 km x 20 km
- Ship traffic follows NW - SE underwater valley, with depth ranging from 10 m to 90 m.
- Daily crossings (ingoing or outgoing)
  - 22 HSC/Catamaran
  - 8-10 Hydrofoil
- A natural laboratory for the study of long waves.
  - Also relevant for tsunami research.

## Summary

- Long wave equations are useful for numerical simulations.
- Several different long wave equations formulated for computation of ship waves.
  - KdV and KP equations preferable for analysis
  - Boussinesq equations preferable for numerical simulations
- The COULWAVE model solves Boussinesq-type equations, and includes several useful features:
  - Open boundary conditions
  - Wetting/drying in coastal zone
  - Wave breaking model
  - Bottom friction models
- COULWAVE model can simulate long wave phenomena on small and large scales: tsunamies, storm surges, ship waves