Standards and Guidelines for Design and Construction of Marine Structures against Seismic and Marine Hazards and Marmaray Project

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FIRST INTERNATIONAL CARIBBEAN WAVES: RISK EVALUATION OF NATURAL HAZARDS IN THE CARIBBEAN

INTRODUCTION

A new seismic design code is being enforced in Turkey, effective September 1, 2008, for transportation structures officially administered by General Directorate for Construction of Railways, Harbors and Airports (RHA) of Ministry of Transportation.

The aim of this contribution is to describe the main aspects of the RHA Seismic Code with special emphasis given to port structures.

The most important aspect of the code rests on its main approach incorporating performance-based design.

In view of a very limited number of seismic codes available for port structures, the new Turkish Seismic Code is expected to attract a special attention with its modern approach. FIRST INTERNATIONAL CARIBBEAN WAVES: RISK EVALUATION OF NATURAL HAZARDS IN THE CARIBBEAN

BASIC APPROACH: PERFORMANCE – BASED DESIGN

The basic design philosophy behind the code is the performance-based design.

As opposed to traditionally used prescriptive strength-based approach, performance-based design rests on an explicit *deformationbased approach*, where damage is *quantified* in terms of inelastic deformation demand quantities on element level under specified multilevel earthquakes.

Such ductile demand quantities are then evaluated against prescribed deformation capacities for selected performance objectives under each earthquake level.

In the mean time internal force quantities corresponding to *brittle* behavior modes are ensured not to exceed the specified *strength capacities*.

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PERFORMANCE – BASED DESIGN PARAMETERS

As in any performance-based design code, the RHA code for port structures starts with the definition of the following performance-based design parameters:

(a) Structural classes associated with the usage, expected performance and functional importance,

(b) Seismic performance levels associated with expected damage levels,
 (c) Earthquake levels associated with frequent, rare and very rare earthquakes,
 (d) Seismic performance objectives under different earthquake levels.

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STRUCTURAL CLASSES

SPECIAL STRUCTURES

- (a) Structures to be used for rapid response and evacuation immediately after an earthquake,
- (b) Structures to be used for toxic, flammable or explosive materials. NOMINAL STRUCTURES
- (a) Structures where the loss of life and property must be avoided,
- (b) Structures of economic and social significance,
- (c) Structures with difficult and time-consuming post-earthquake repair and retrofit needs,

SIMPLE STRUCTURES

- (a) Less important structures other than those classified in Special and Nominal Structures,
- (b) Structures other than those classified as Unimportant Structures.

UNIMPORTANT STRUCTURES

- (a) Easily replaceable structures,
- (b) Structures not causing life safety risk even extensively damaged,
- (c) Temporary structures.

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SEISMIC PERFORMANCE LEVELS

MINIMUM DAMAGE (MD) PERFORMANCE LEVEL

corresponds to a state where no or a very limited damage occurs in port structures and/or in their elements. In this case, port operation continues uninterrupted or if any, service interruptions are limited to few days.

CONTROLLED DAMAGE (CD) PERFORMANCE LEVEL

corresponds to a state where non-extensive, repairable damage occurs in port structures and/or in their elements. In this case, short-term (few weeks or months) interruptions in related port operations may be expected.

EXTENSIVE DAMAGE (ED) PERFORMANCE LEVEL

corresponds to a state where extensive damage occurs in port structures and/or in their elements. In this case, long-term interruptions or even closures in related port operations may be expected.

STATE OF COLLAPSE (CS)

corresponds to the collapse state in port structures and/or in their elements. Related port operation is terminated. FIRST INTERNATIONAL CARIBBEAN WAVES: RISK EVALUATION OF NATURAL HAZARDS IN THE CARIBBEAN

EARTHQUAKE LEVELS

(E1) Earthquake Level

represents relatively frequent but low-intensity earthquake ground motions with a high probability to occur during the service life of port structures. The probability of exceedance of (E1) level earthquake in 50 years is 50%, which corresponds to a return period of 72 years.

(E2) Earthquake Level

represents the infrequent and high-intensity earthquake ground motions with a low probability to occur during the service life of port structures. The probability of exceedance of (E2) level earthquake in 50 years is 10%, which corresponds to a return period of 475 years.

(E3) Earthquake Level

represents the highest intensity, very infrequent earthquake ground motions that port structures within the scope of the code may be subjected to. The probability of exceedance of (E3) level earthquake in 50 years is 2%, which corresponds to a return period of 2475 years.

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MINIMUM PERFORMANCE OBJECTIVES

Port Structure Class	(E1) Earthquake Level	(E2) Earthquake Level	(E3) Earthquake Level
Special		MD	CD
Nominal	MD	CD	(ED)*
Simple	CD	(ED)*	
Unimportant	(ED)*	(CS)*	

* Implied objectives not requiring design verification.

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ANALYSIS AND DESIGN PROCEDURES

Being a performance-based code, the new seismic code for port structures mainly rests on a *deformation-based design (DBD)* approach, which requires the implementation of nonlinear seismic analysis procedures. However, linear analysis procedures within the framework of traditional *strength-based design (SBD)* are also allowed for the verification of *Minimum Damage (MD) Performance Objective* where structural behavior is at or near the elastic limits.

(CD) Performance Objective with relatively conservative design parameters.

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APPLICABLE DESIGN APPROACHES TO PORT STRUCTURES

Port Structure Class	<i>(E1) Earthquake Level</i>	(E2) Earthquake Level	<i>(E3) Earthquake Level</i>
Special	-	SBD / DBD	DBD
Nominal	SBD	SBD / DBD	
Simple	SBD		
Unimportant	-		-

NEW TURKISH SEISMIC DESIGN CODE FOR PORT STRUCTURES: A PERFORMANCE-BASED APPROACH

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INTRODUCTION

New Turkish Code for Coastal and Port Structures

A seismic design code has been published in the Official Gazette of Contents; 1-Earthquake code for coastal and port structures Turkish Republic on 18 August 2007 which will be applicable to 2-Coastal and Port Structure Design Code

transportation structures administered by the General Directorate for 3-Geotechnical Code

Construction of Railways, Harbors and Airports (RHA) of Ministry of 4-Material, Construction, Control and Maintanence Code

Transportation. The important aspect of the code rests on its main

approach incorporating "performance-based design" (PIANC, 1997). CLASSIFICATION OF PORT STRUCTURES

First, port structures have been classified with respect to their anticipated seismic performance, usage and functional importance leading to classes of "special", "nominal", "simple" and "unimportant" structures.

PERFORMANCE LEVELS

Standard performance levels for port structures have been specified

- terms of different damage levels: a) Minimum Damage (MD) Level b) Controlled Damage (CD) Level c) Extensive Damage (ED) Level
- d) Collapse State (CS)

SEISMIC GROUND MOTION LEVELS

Three levels of design earthquakes E1, E2 and E3 have been specified Two different design methods have been specified, namely, Strength-Based Design with return periods of 72, 475 and 2475 years, corresponding to 50%, (SBD) Method and Deformation-Based Design (DBD) Method. As an example, 10% and 2% probability of exceedance in 50 years, respectively. Table 2 shows the use of such methods in Spectral accelerations at 0.2 second and 1.0 second have been given piled pier and wharf structures.

for all coastal regions in the country.

MINIMUM PERFORMANCE OBJECTIVES

structure under different earthquake levels as shown in Table 1.

Sructure Class	(E1) Earthquake Level	(E2) Earthquake Level	(E3) Earthquake Level
Special	-	MD	CD
Nominal	MD	CD	ED*
Simple	CD	ED*	-
Unimpor	ED*	CS*	
"Implied objectives"	not requiring verification	on.	
Table Sructure Class	1. Use of Design (E1)	Methods objecti (E2)	ves (E3)
	Earthquake Level	Earthquake	Earthquake Level
Special	-	SBD/DBD	DBD
Nominal	SBD	DBD	-
Simple	SBD	-	-
Unimpor	-		-
1973	Table 3 Saismic	Load Reduction	Factors
	Table 5. Seisinie		
Pile Arrangeme	nt	Performance	
Pile Arrangeme	nt MD	C	D
	nt		D

Strength-Based Design (SBD) Method based on linear analysis with reduced Minimum performance objectives are specified for each class of seismic loads is generally employed to verify the Minimum Damage (MD) performance objective. As an example, Seismic Load Reduction Factors (R) are given in Table 3 for piled pier and wharf structures.

> Deformation-Based Design (DBD) Method based on nonlinear analysis is essentially used in "nominal" and "special" structures to verify the Controlled Damage (CD) performance objective. Recommended nonlinear analysis procedures include response-history analysis in time domain as well as singlemode and multi-mode pushover analyses. In piled structures, soil is modeled with nonlinear p-y, t-z and P-Z springs. Inelastic deformantion demands obtained from nonlinear analysis are verified against the corresponding capacities defined for various performance objectives. Strain capacities are given in Table 4 for pile sections.

e REFERENCE

PIANC(1997), Seismic Design Guidelines for Port Structures, A.A.Balkema Publishers.

Strain	Performance Level	
	MD	CD ²
Conc. Strain in RC Piles	0.004	0.020/008
Rebar Strain in RC Piles	0.010	0.040/0.01
PS Strain in RC Piles	0.005^{1}	0.040/0.01
Strain in Steel Piles	0.008	0.030/0.01
¹ Strain increment due to earthquake		
² Figures on right for underground str	ructures	



DESIGN METHODS

FIRST INTERNATIONAL CARIBBEAN WAVES: RISK EVALUATION OF NATURAL HAZARDS IN THE CARIBBEAN

Coastal and Port Structure Design Code
Geotechnical Code
Material, Construction, Control and Maintanence Code

Marmaray Project





Employer's Representative

Pacific Consultants International
Yüksel Proje Uluslararası A.Ş.
Japan Railway Technical Services
Oriental Consultants Co. Ltd.
Subcontractors

- Parsons Brinckerhoff International Inc.
- Terzibaşıoğlu Müşavir Mühendislik Ltd.
- Sial Yerbilimleri Etüd ve Müşavirlik Ltd.

3 separate Contracts

- The Bosphorus Crossing (BC1)
 - Immersed Tube Tunnel under the Bosphorus
 - Bored Tunnels under the City on both sides
 - 4 new Stations (Kazliceşme, Yenikapı, Sirkeci and Uskudar)
- The Upgrading of the Commuter Rail (CR1)
 - A third track (for IC and freight) on surface and full upgrading of existing tracks and Stations
 - New Signaling, Communication, Fare collection, Operations Control Centre etc.
- New Rolling Stock (CR2)
 - 44 number of 10 car trains



Total length of Commuter Rail is app. 77 km: At grade, European side 19.6 km At grade, Asian side 43.4 km Bored tunnels 12.2 km Immersed tube tunnel 1.4 km

From Halkali to Gebze

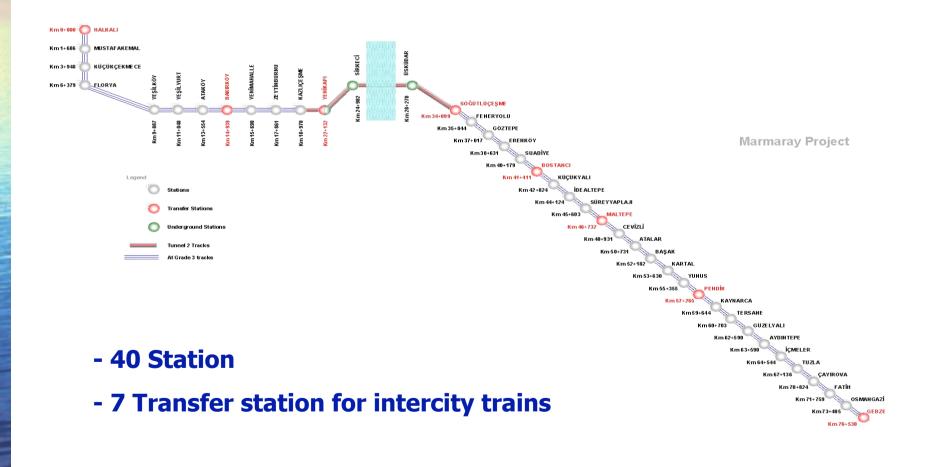
BC1 ALINGMENT PROFILE





Schematical Alinment Plan Halkali Atakoy Yedikule Haydarp. Pendik Gebze : At-grade : Tunnel

Marmaray Stations

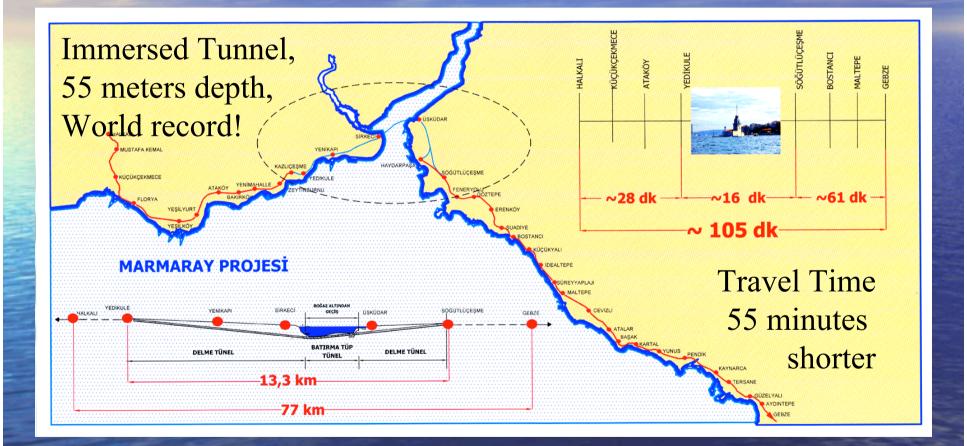


The Benefits of the Project

The Project will:

- Create long-term solution to transportation problems of Istanbul
- Have a capacity of 75.000 passengers per hour per direction
- Reduce impacts of Car Traffic in the old City
- Reduce congestion on the existing bridges
- Connect the Railway from Europe to Asia and visa versa
- Decrease pollution in Istanbul, decrease CO₂ release
- Decrease travel time for more than 1 million people every day

Alignment and Travel Time



Travel time between Gebze & Halkalı will be 55 min shorter. The travel time between Üsküdar and Sirkeci will only be 4 minutes.

Employer's Requirements Design & Build type of Contract Fitness for purpose (functional requirements) Minimum requirements - Design - Materials - Workmanship Balanced" requirements, room for variations

Marmaray Project Total Costs, Full Project, 1999 Estimate

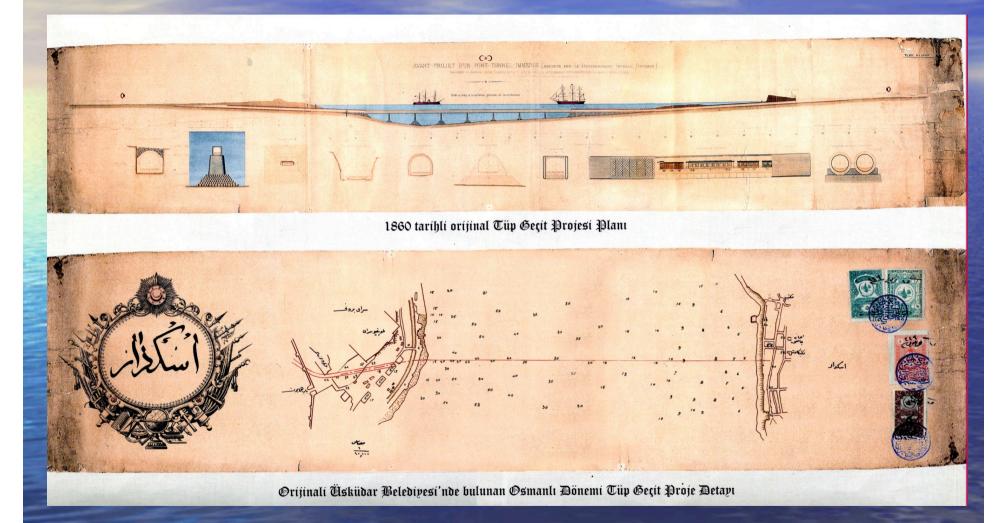
Торіс	Million US\$
Bosphorus Crossing and CR1 Civil	1.100
Commuter Rail, Rolling St. and E&M	1.500
Grand Total, approximately	2.600

The Bosphorus Crossing (BC1)

The Contractor
Taisei Corporation, Lead Partner, Japan
Gama, Turkey
Nurol Insaat, Turkey

Contract Price: 823 million USD Commencement date: 27th August 2004

The Background (or history)



Year 1860 Engineer S.Preault

Sarayburnu - Üsküdar



Marmaray Project

A dream of 150 years

Year 2004

Sarayburnu - Üsküdar

Challenging Project

Deepest Immersed Tunnel

Heavy Sea Traffic Area

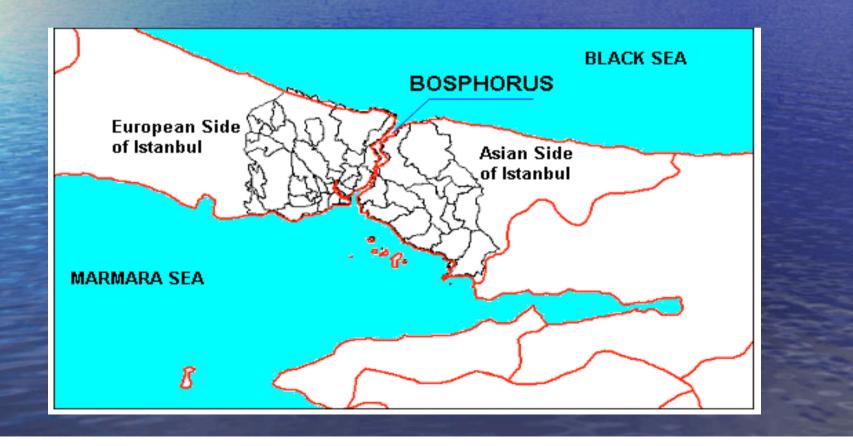
Stratified Currents up to 5 knots

Earthquake Zone

 The Bosphorus Strait is a pathway between Marmara and Black seas.

 Its width varies between 0.7 and 3.5 km with average value of 1.3 km at the surface.

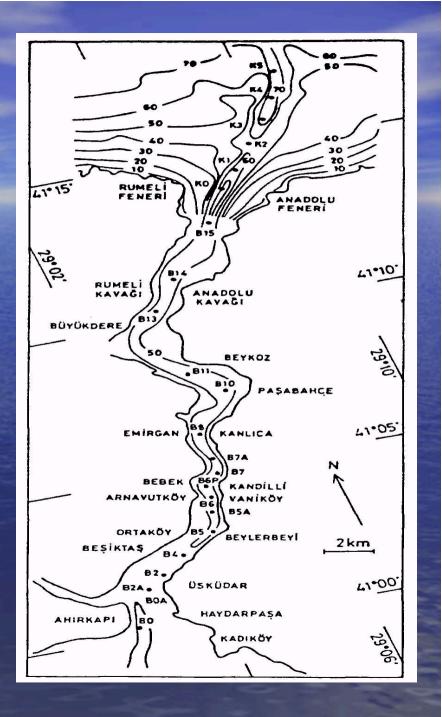
• The depth varies in the range of 30 and 100 m.

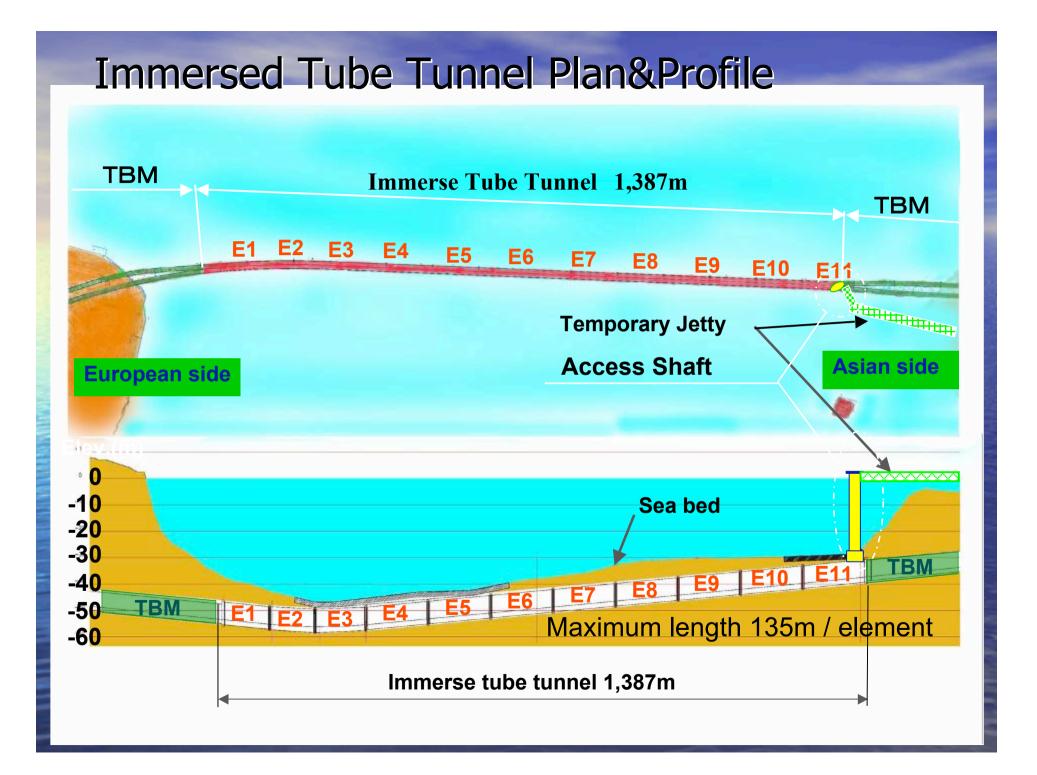


The flow in Bosphorus Strait is a strongly two stratified two-layer system:
(1) an upper-level current that flows south from the Black Sea to the Sea of Marmara; and
(2) a lower-level current that flows north from the Sea of Marmara to the Black

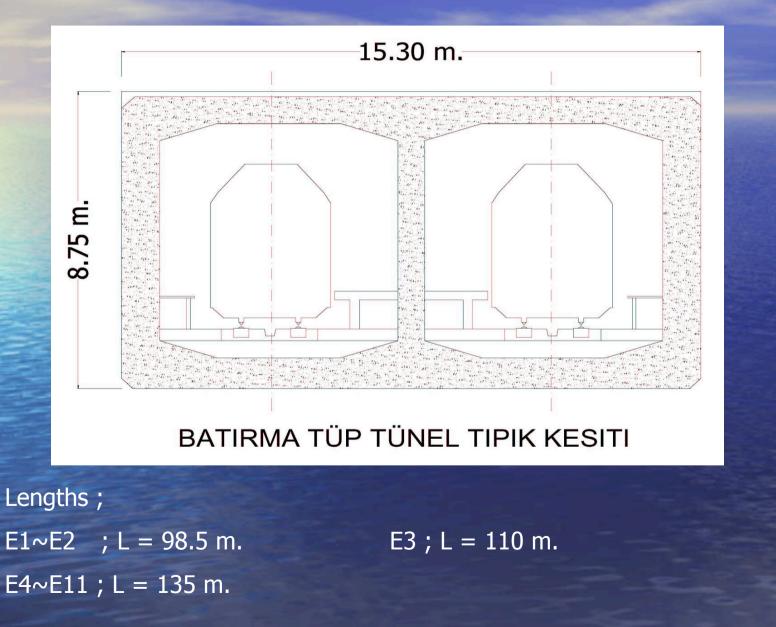
Sea.

 The stratified current is controlled by mainly two reasons which are density and water depth differences. The Bosphorus Strait has significant variations in width and depth along its length. • Two sills located near the both entrance regions. The sills inlfuences the flow characteristics within the Bosphorus.





Typical Cross-section of IMT



Design

Loads

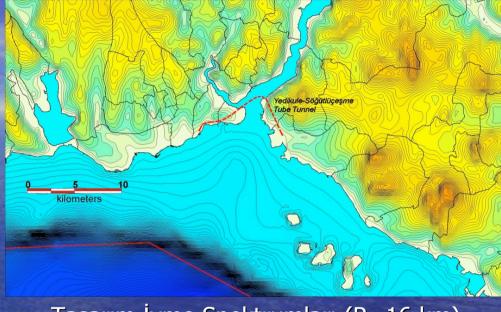
- Dead and Live Loads
- Train load (UIC-S1950)
- Hydrostatic loads
- Current effect
- Ground Loads
- Differential Settlement
- Temperature Effects
- Fire
- Explosion Load
- Train Derailment Load
- Falling and Dragging Anchors
- Sunken Ship Effect
- Seismic Loads.

Seismic Design Performance Requirements for Bosphorus Crossing

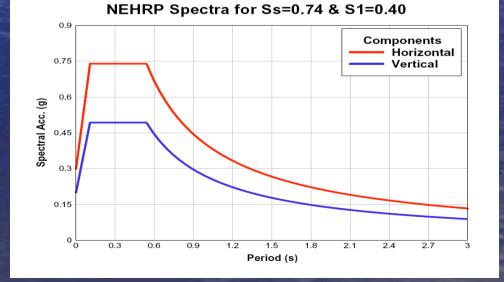
Design Basis Earthquake (Moment Magnitude : Mw=7.5)

Performance Criteria ;

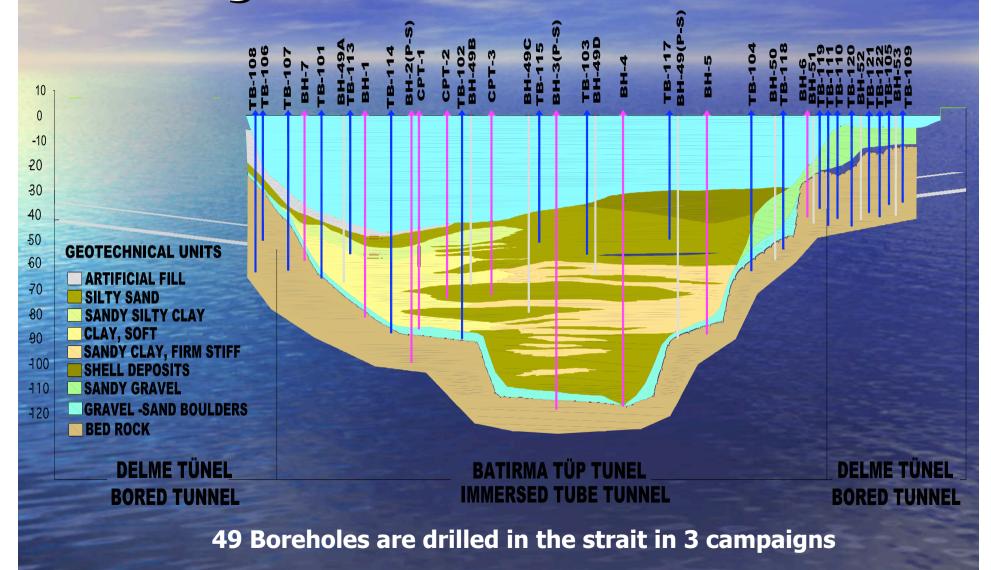
- No Risk to Life Safety
- Minimum Risk of Losing Functionality (normal operation can be quickly resumed)
- Minor and Easily Repairable
 Damage to Structural
 Elements
- Minimum inelastic
 Deformations
- Immersed Tunnel and Joints Remain Watertight



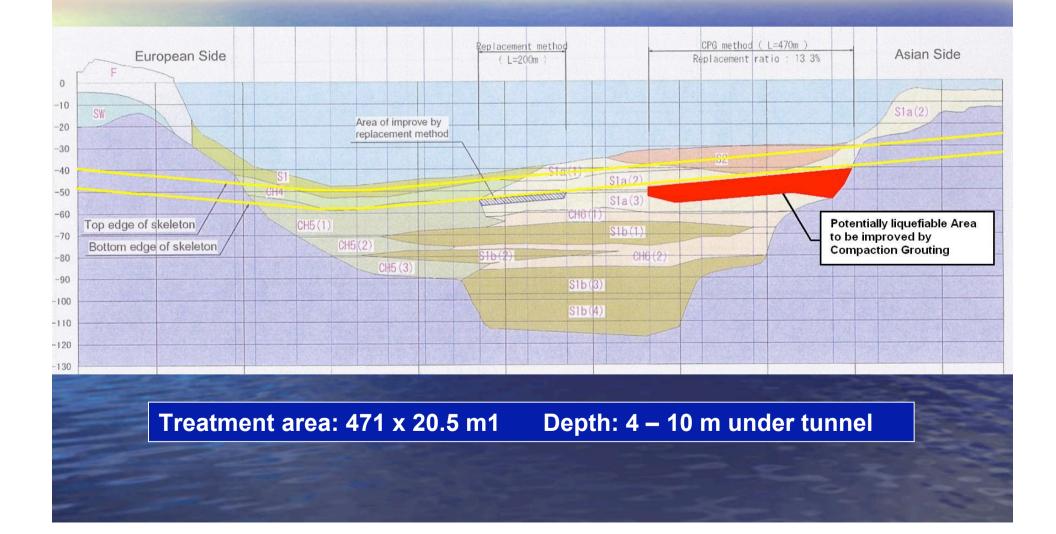
Tasarım İvme Spektrumları (R=16 km)



Geological Profile of the Strait



Ground Improvement Works

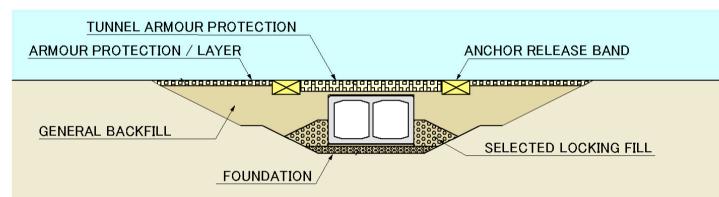


Dredging Works

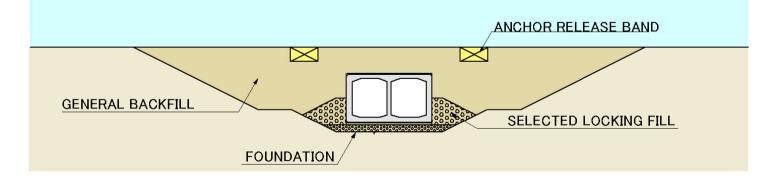


Dredging Works





BACK FILL THICKNESS IS OVER 4m



Contaminated soil: 120.000 m3 Clean soil: 1.000.000 m3 Stone backfill: 130.000 m3

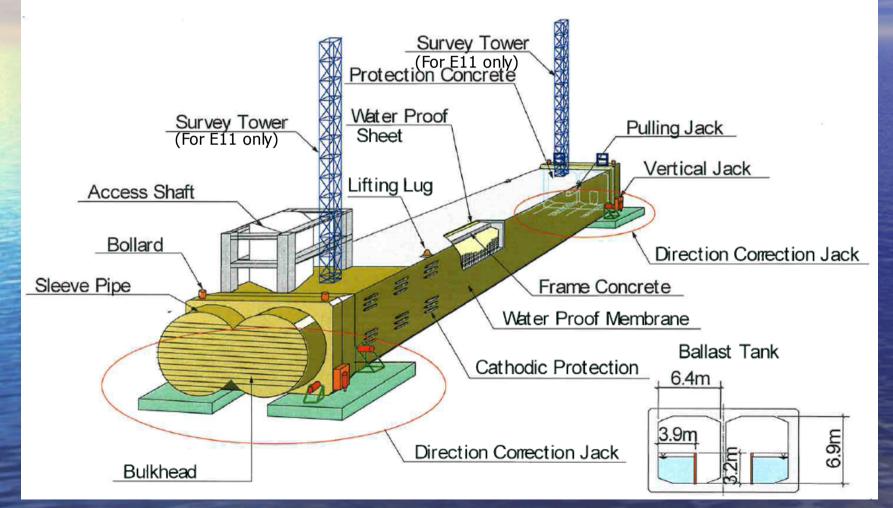
Soil backfill: 800.000 m3

Confined Disposal Facility



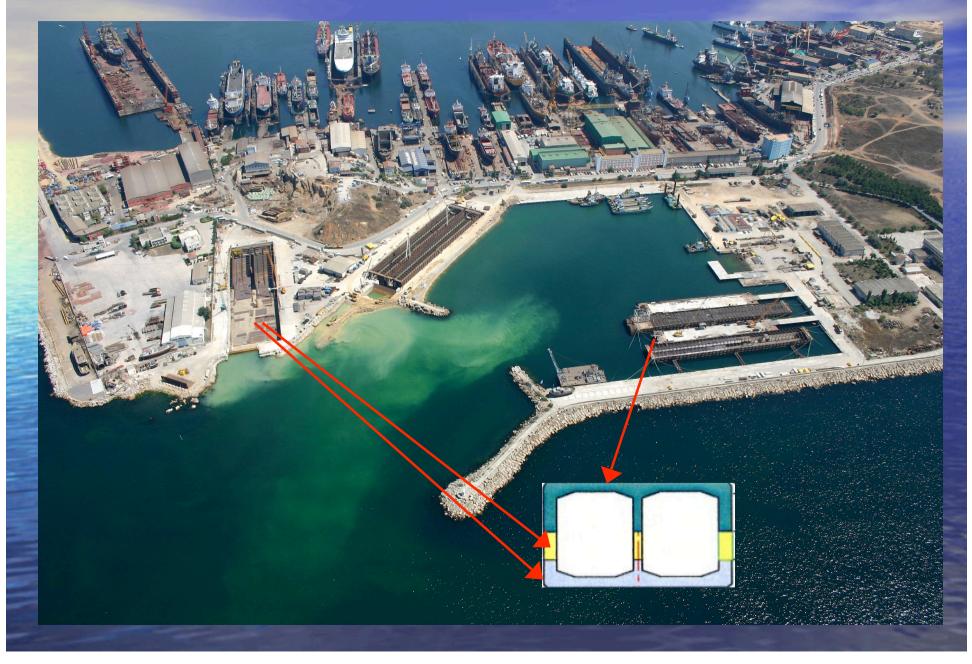
Immersed Tunnel

Arrangement Plan of Outfitting for Element-11

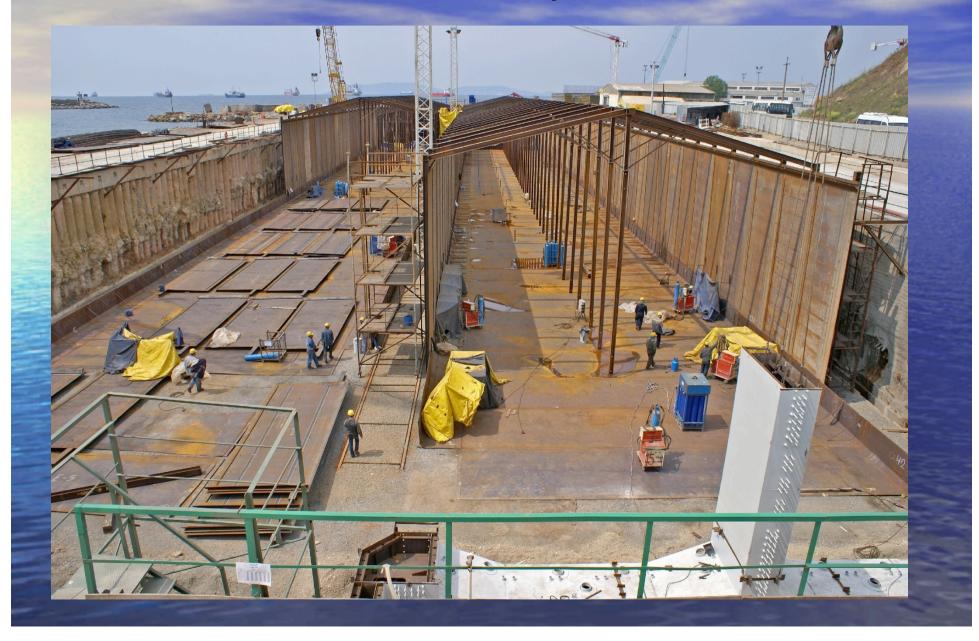


Typical Dimensions $135m \times 15.5m \times 8.6m$, Weight = 19,000-20,000 ton

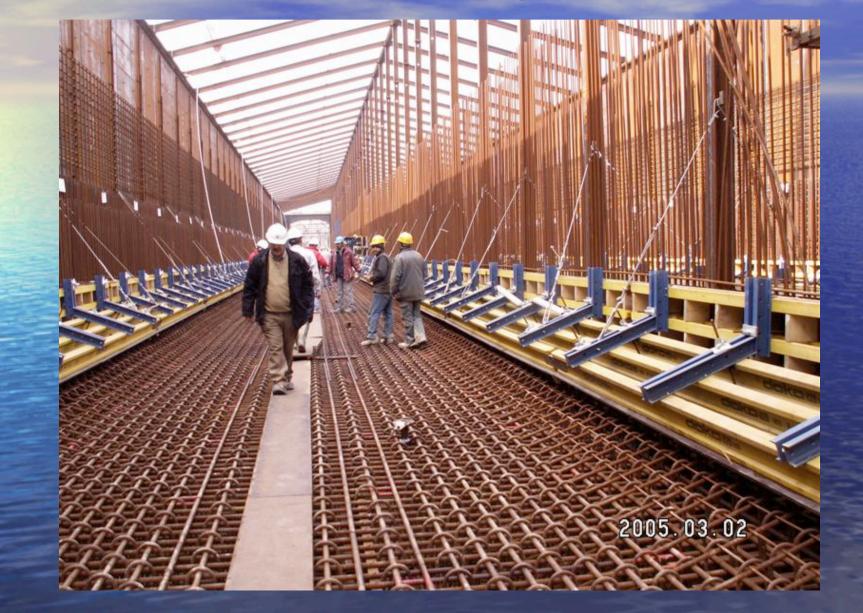
Tuzla Offshore Element Fabrication Site



Element Fabrication in Dry Dock



Element Fabrication in Dry Dock



Elemanların yüzdürülerek Boğaza götürülmesi Location of Go / No Go Decision for Immersion

Immersion Location

Route of Lowing

Before enter the Ship way Go / No go decision by forecast at 0:00

Final Decision Location

First Decision

Using forecast at 12:00

Second Decision

Before sail

Using measuring current in Immersion Water at 18:00

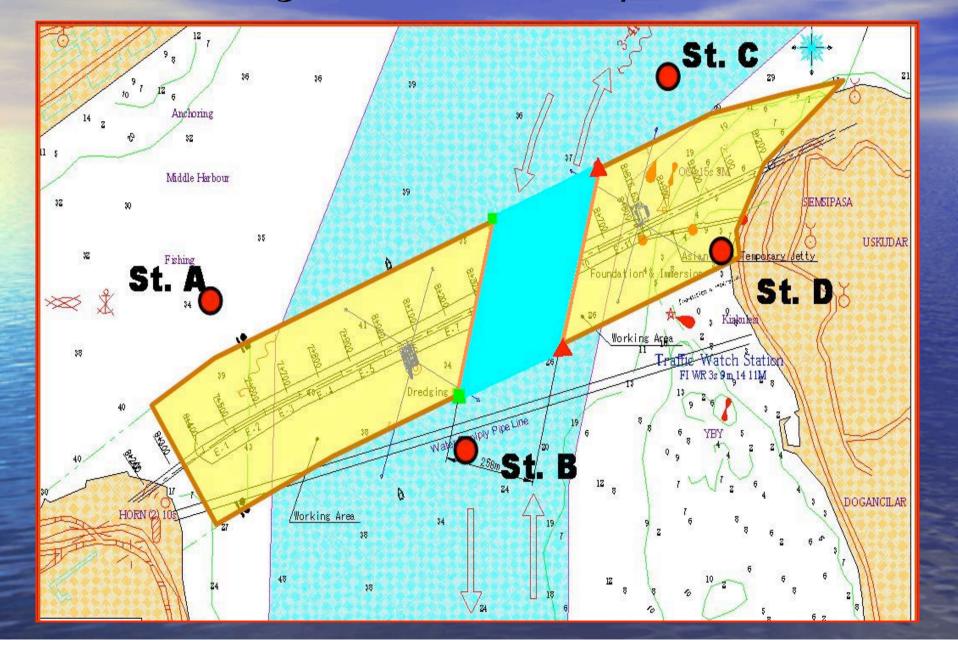
Decision Location before Towing

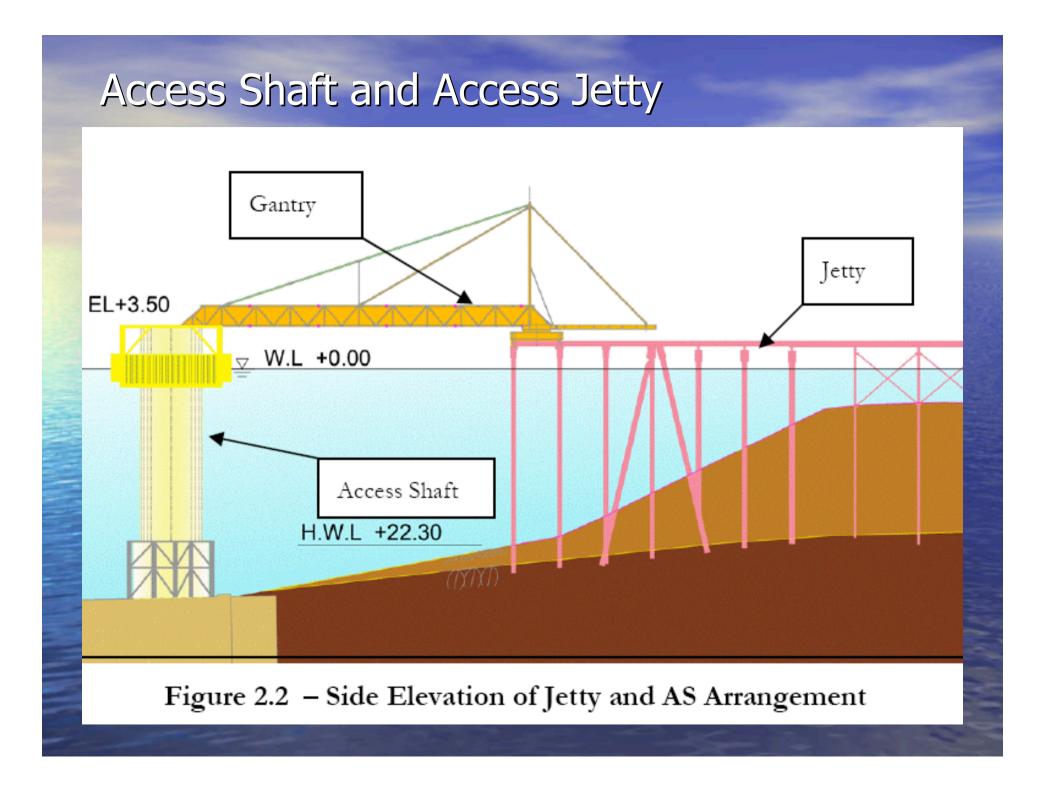
Final Outfitting Location

Manufacturing Area

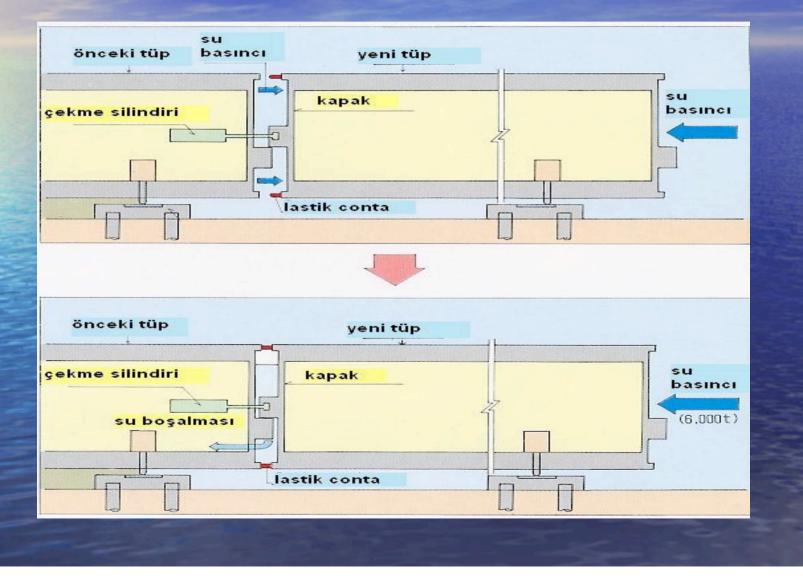
Route of Towing the Element(10.8km)

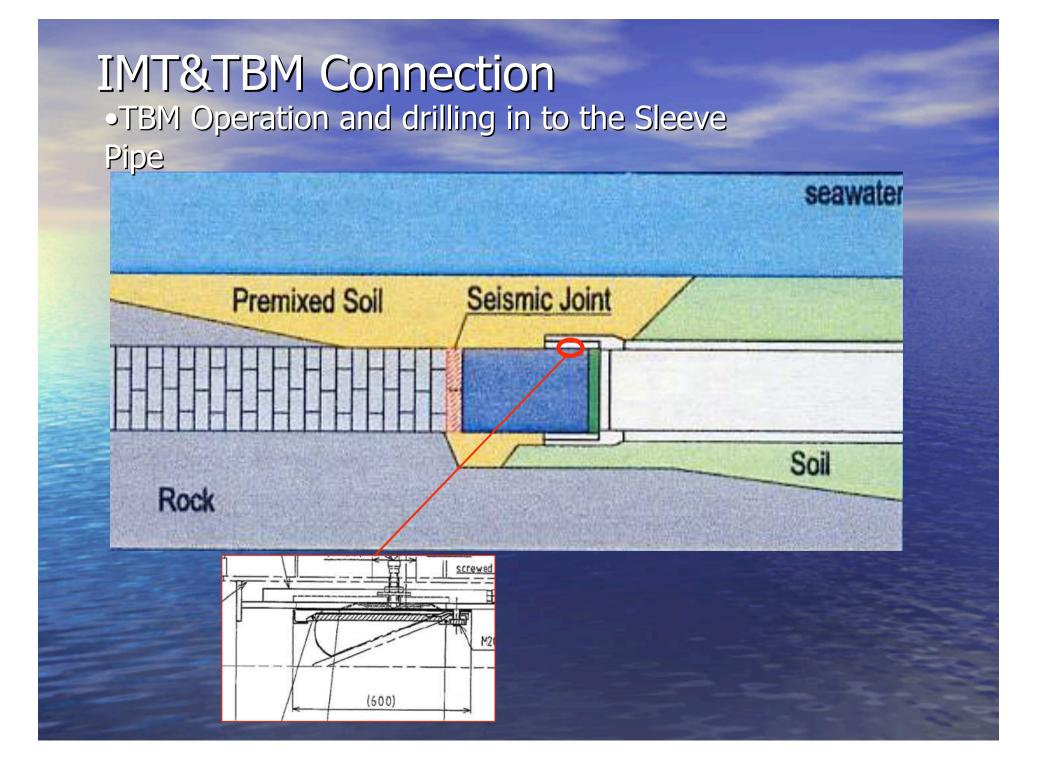
Traffic Management in the Bosphorus



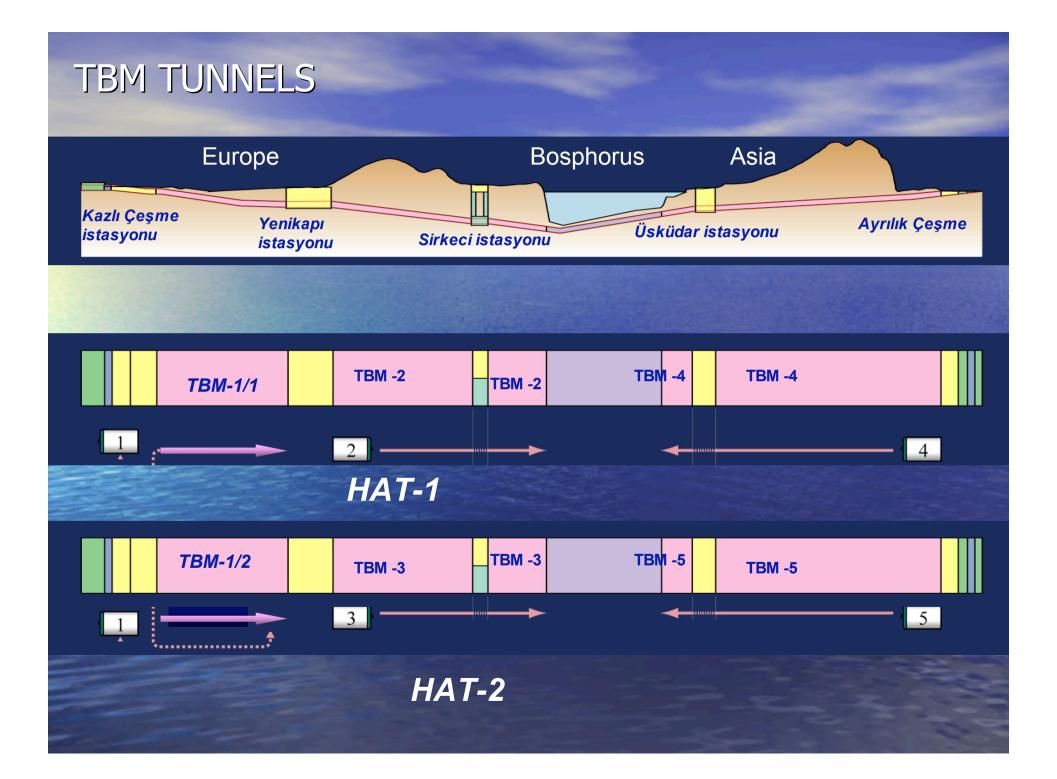


Connection of the Immersed Elements "automatic" hydraulic connection









TBM1 (EPB TYPE, YEDIKULE-YENIKAPI)



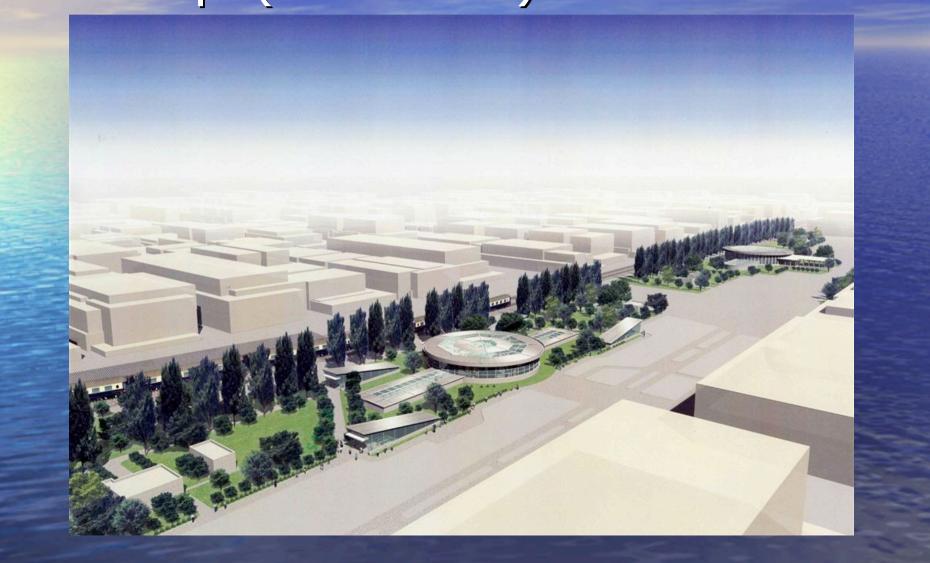
TBM4&5 (SLURRY TYPE, AYRILIKÇEŞME-ÜSKÜDAR)



TBM SEGMENTS



BC1 Underground Stations, Yenikapı (Cut&cover)



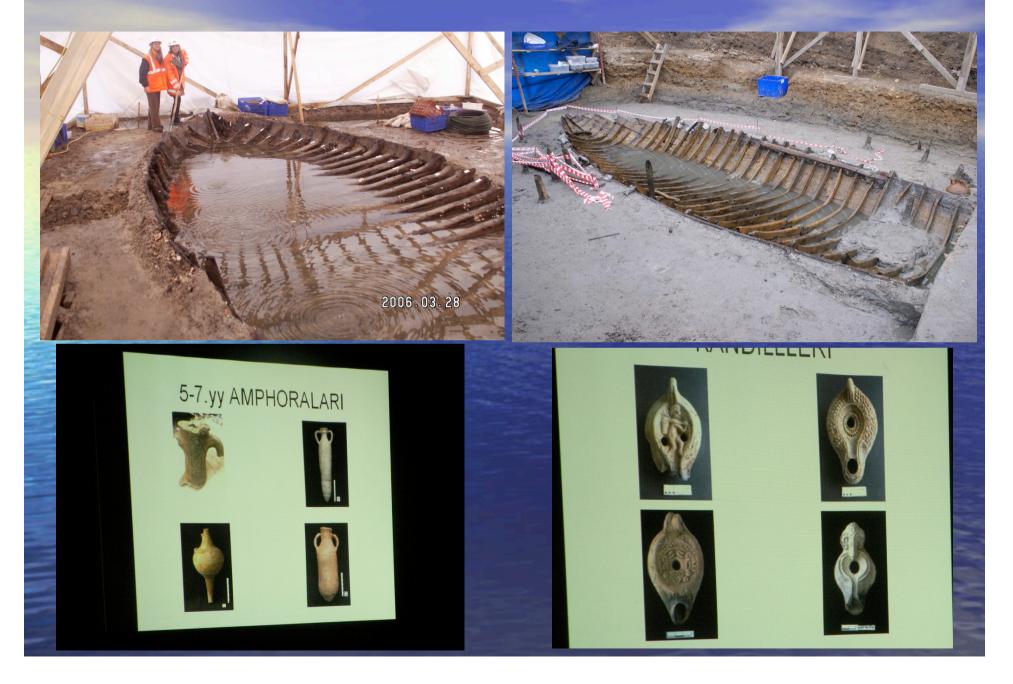
BC1 Underground Stations, Yenikapı (Cut&cover)

Potansiyel Dizayn, Yenikapi Transfer İstasyonu

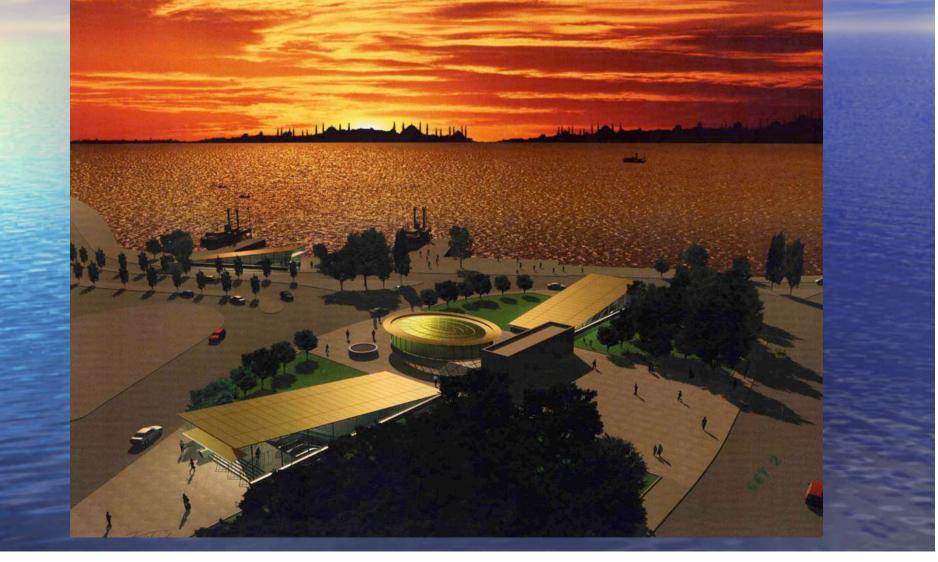
Yenikapı Station Area – Archaeological Excavation



Yenikapı Station Area – Archaeological Excavation



BC1 Underground Stations, Üsküdar (Cut&cover)









www.marmaray.com



The Maiden's Tower in the Istanbul Strait